

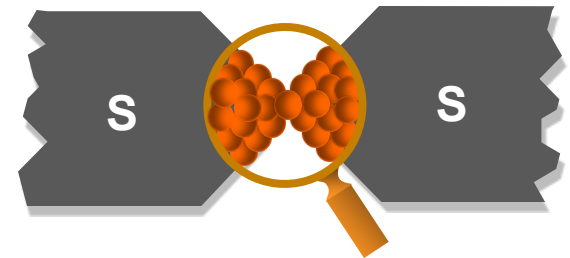
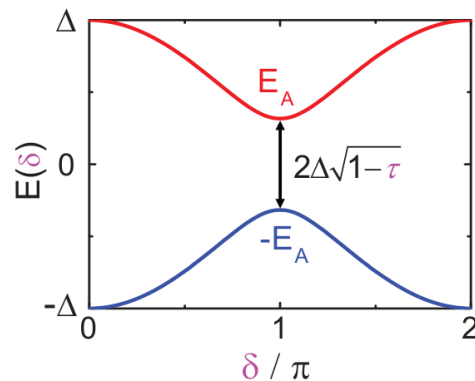
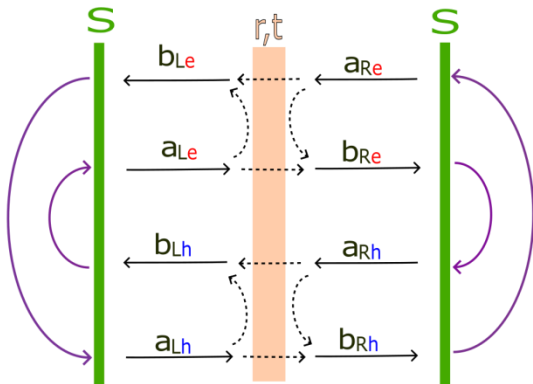


# Andreev Bound States

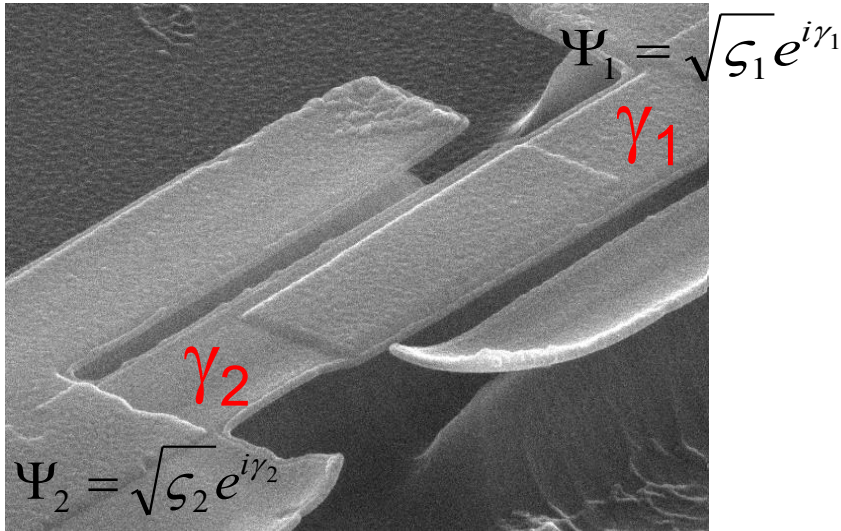
**Maciej Zgirski**

Institute of Physics of the Polish Academy of Sciences, **MagTop**, **CoolPhon Group**

Summer School: Physics of Quantum Chips, University of Gdańsk, 03/07/2025

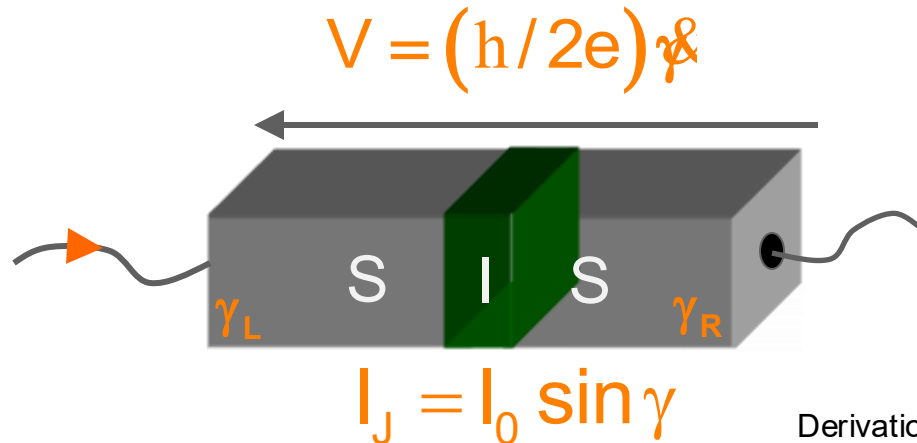


# Josephson relations



$$I = I_0 \cdot \sin(\gamma_2 - \gamma_1)$$

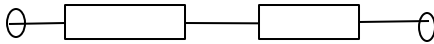
$$\frac{d(\gamma_2 - \gamma_1)}{dt} = \frac{2 \cdot e}{\hbar} \cdot V$$



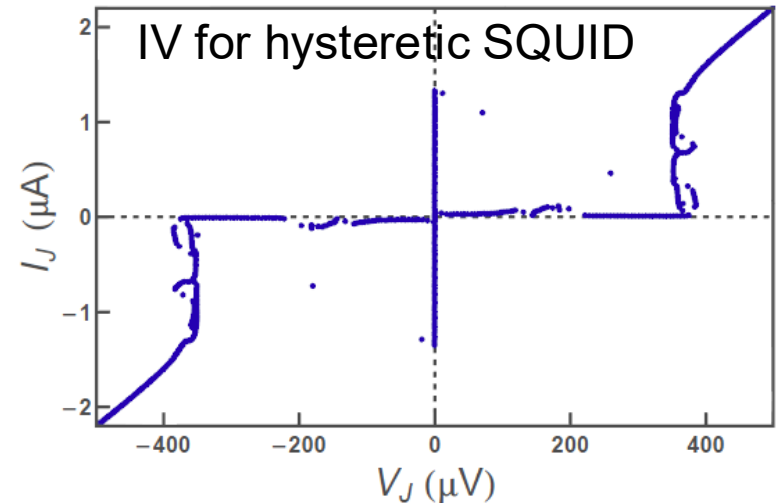
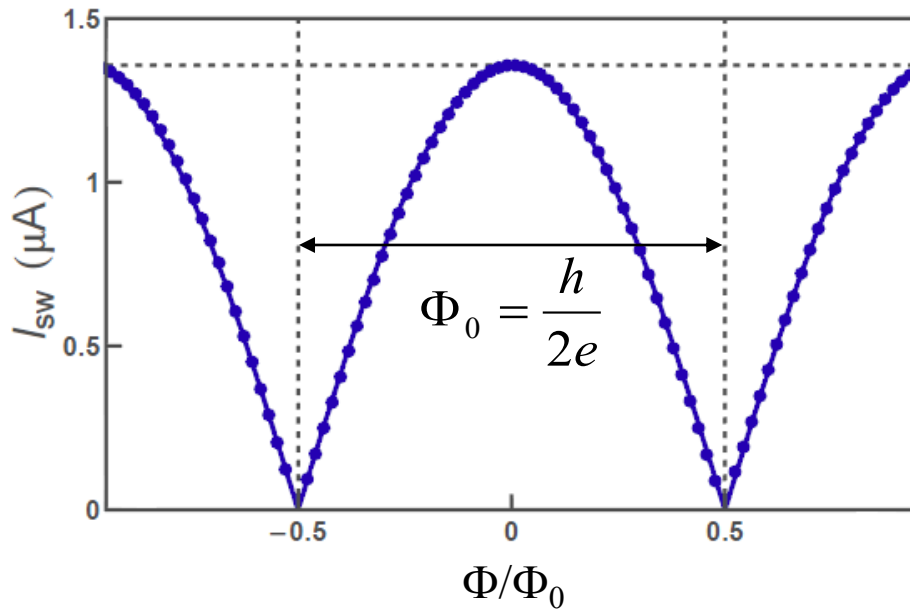
Derivation of Feynman relations:

Feynman, vol. III, seminar on superconductivity

# Voltage vs. phase

Normal metal	Superconductor
Voltage drop forces current	Phase drop imposes current
<p><math>R</math>      <math>r \ll R</math></p>  <p>All voltage drops on <math>R</math></p>	<p>The biggest phase drop in the loop on the weakest weak link</p>

# Interference pattern for SQUID



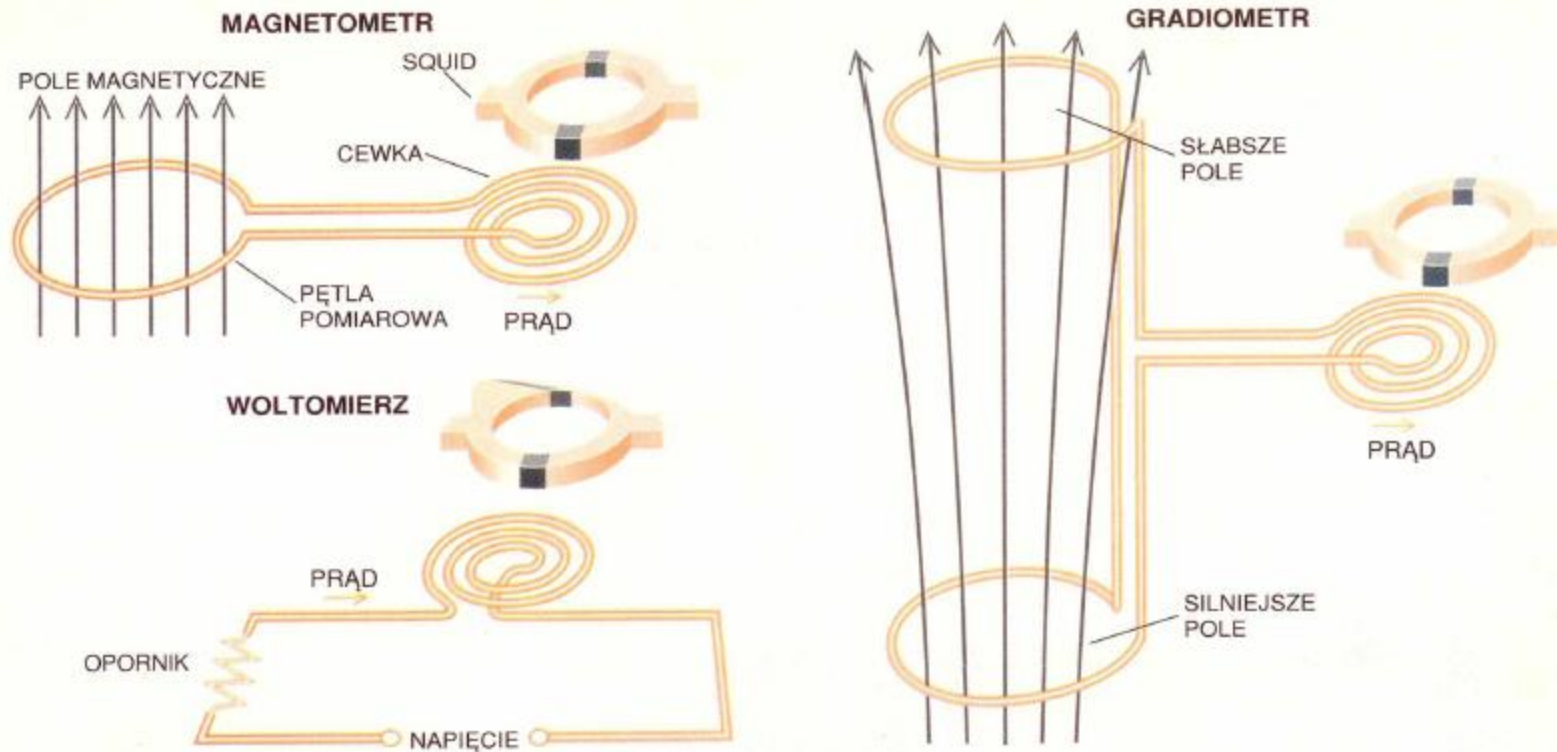
Symmetric SQUID is superconducting analog of double slit optical (or electron) interferometer:

applied flux –  $\Phi \Leftrightarrow d \cdot \sin\theta$  - path difference

Flux quantum –  $\Phi_0 \Leftrightarrow \lambda$  – wavelength

For symmetric SQUID (2 x JJ): 
$$I_c = 2 \cdot I_{JJ}^0 \cdot \left| \cos\left(\pi \cdot \frac{\Phi}{\Phi_0}\right) \right|$$

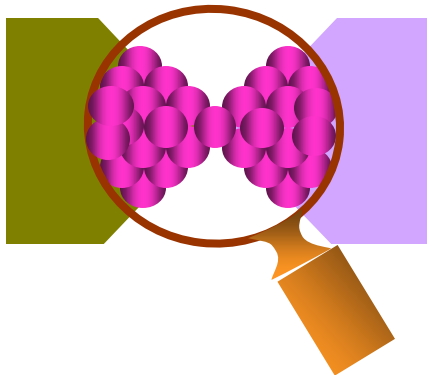
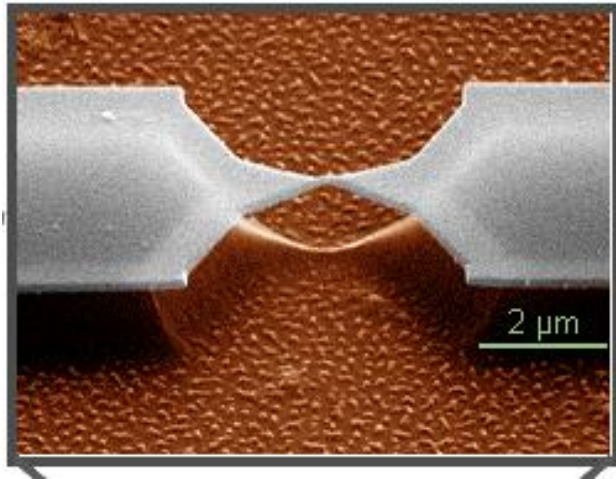
# SQUID – various applications



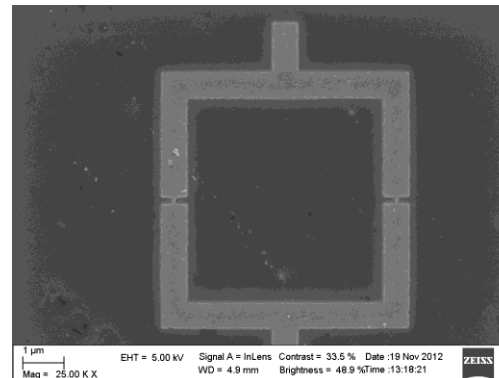
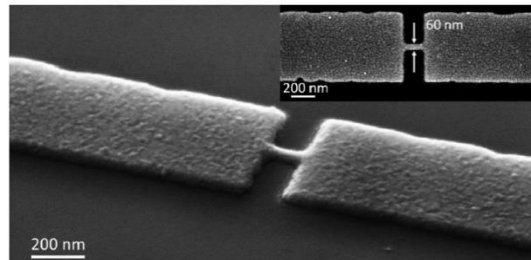
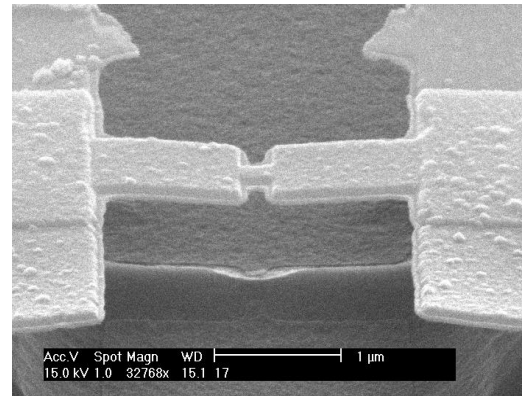
URZĄDZENIA WYKORZYSTUJĄCE SQUID zwykle wymagają dodatkowych elementów. Magnetometr zawiera „transformator strumienia”, który składa się z pętli pomiarowej połączonej z cewką sprzężoną z interferometrem. Pole magnetyczne wzbudza prąd w pętli, powodując jego przepływ przez cewkę i powstanie strumienia pola magnetycznego przenikającego interferometr. W gradiometrze dwie oddalone od siebie pętle pomiarowe nawinięte w przeciwnych kierunkach są poddawane jednoczesnemu działaniu pola magnetycznego. Strumień pola magnetycznego przenika interferometr tylko wtedy, gdy natężenie tego pola w obu pętlach jest różne. W woltomierzu mierzone napięcie wywołuje przepływ prądu o natężeniu równym ilorazowi wartości tego napięcia i wielkości oporu połączonego z cewką sprzężoną z nadprzewodnikowym interferometrem kwantowym.

# ZOO of Josephson junctions

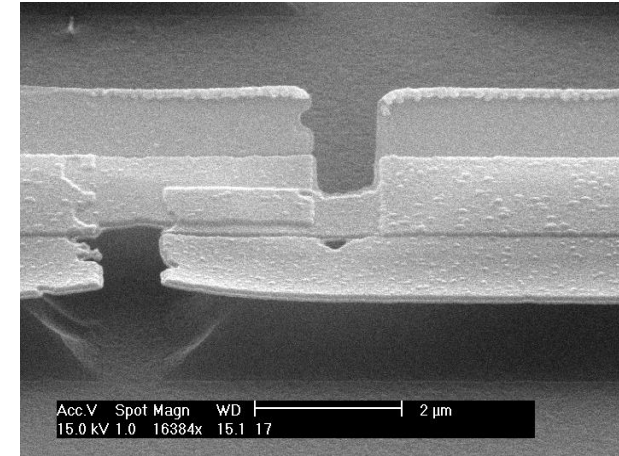
Atomic point contact



Diffusive weak link



Tunnel junction

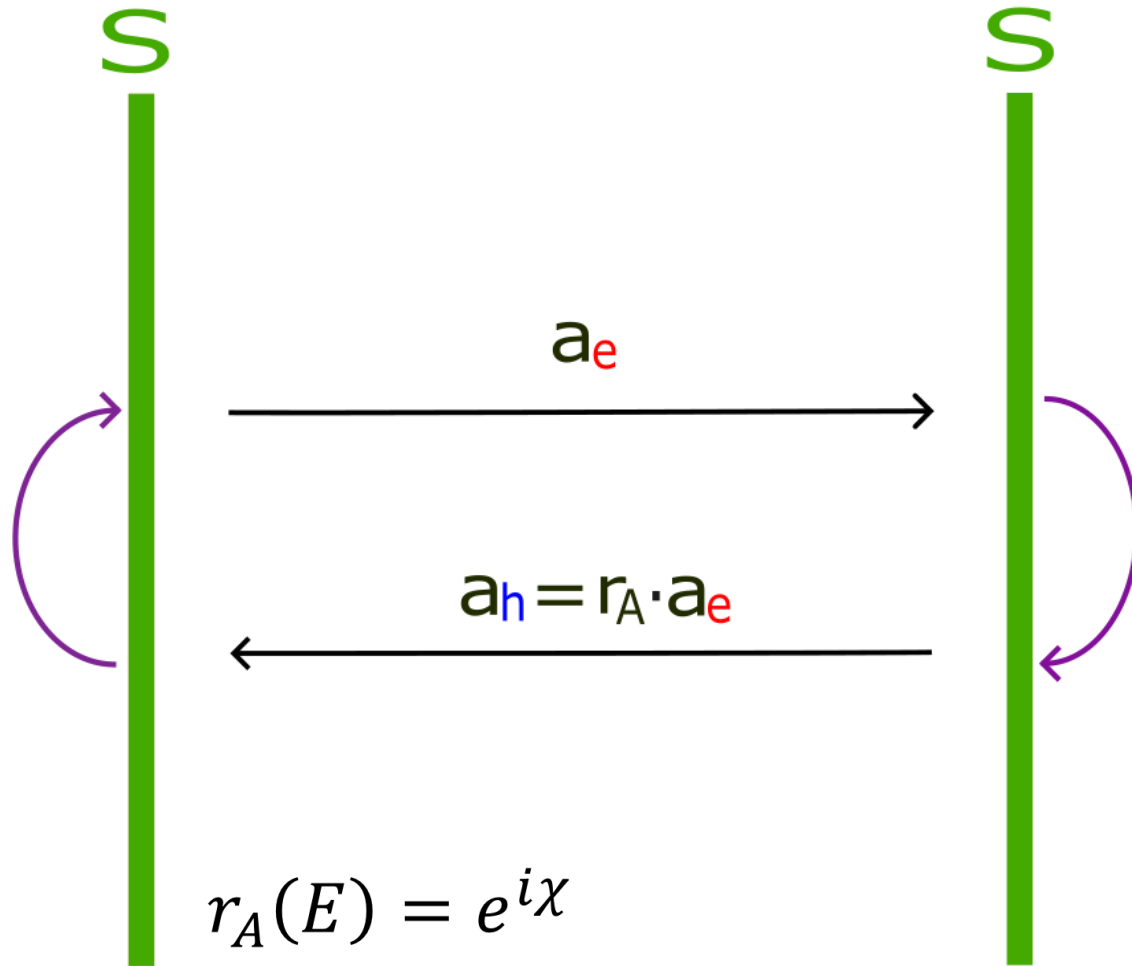


Note: The famous 1st Josephson relation holds only for tunnelling junctions.

But it can be extended to treat all types of JJ !!!

⇒ We will need  
ANDREEV BOUND STATES  
(our next lecture)

# Andreev Reflection

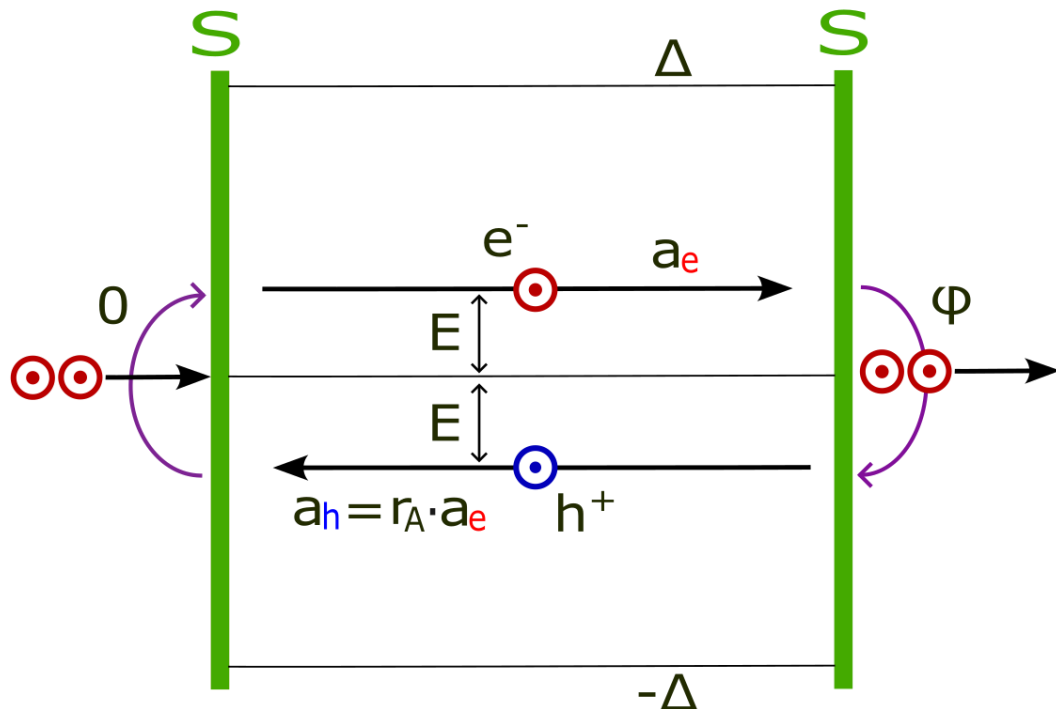


$$r_A(E) = e^{i\chi}$$

$$\chi = -\arccos\left(\frac{E}{\Delta}\right) - \varphi$$



# Andreev Reflection



Constructive interference happens when:

$$\chi_{h \leftarrow e} + \chi_{e \leftarrow h} = 2\pi$$

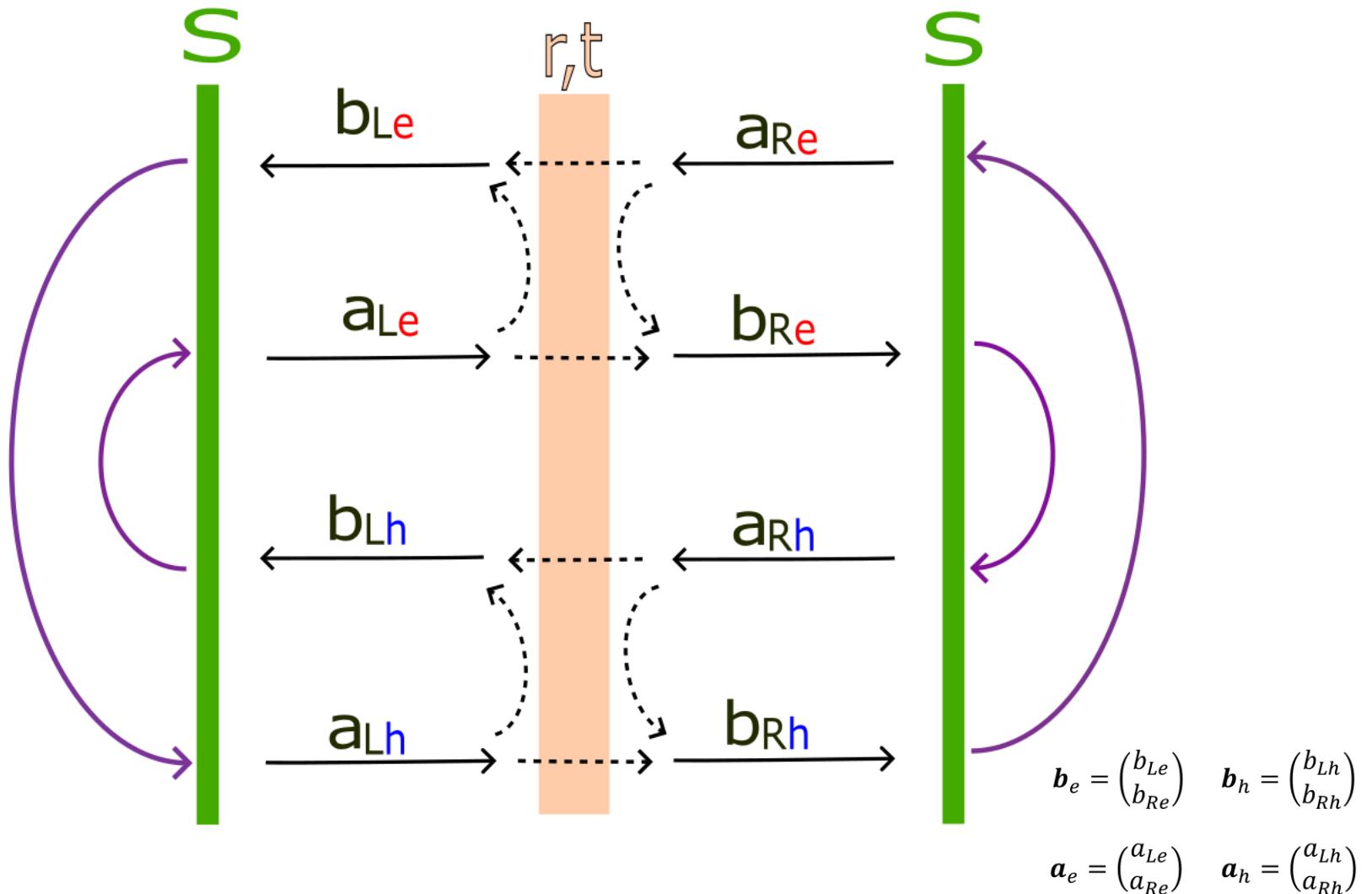
$$\chi_{h \leftarrow e} = -\arccos\left(\frac{E}{\Delta}\right) - \varphi$$

$$\chi_{e \leftarrow h} = -\arccos\left(\frac{E}{\Delta}\right) + 0$$

$$r_A(E) = e^{i\chi}$$



# Superconducting Junction



## Normal scattering

$$\hat{s}_e = \begin{pmatrix} \sqrt{R}e^{i\theta} & \sqrt{T}e^{i\eta} \\ \sqrt{T}e^{i\eta} & -\sqrt{R}e^{i(2\eta-\theta)} \end{pmatrix}$$

$$\hat{s}_h = \hat{s}_e^*$$

$$\mathbf{b}_e = \begin{pmatrix} b_{Le} \\ b_{Re} \end{pmatrix} = \hat{s}_e \begin{pmatrix} a_{Le} \\ a_{Re} \end{pmatrix}$$

$$\begin{pmatrix} \mathbf{b}_e \\ \mathbf{b}_h \end{pmatrix} = \begin{pmatrix} \hat{s}_e & 0 \\ 0 & \hat{s}_h \end{pmatrix} \begin{pmatrix} \mathbf{a}_e \\ \mathbf{a}_h \end{pmatrix}$$

Tells how a amplitudes  
are converted into b amplitudes

## Andreev Reflection

$$\hat{s}_{he} = \begin{pmatrix} e^{i\chi_{heL}} & 0 \\ 0 & e^{i\chi_{heR}} \end{pmatrix}$$

$$\hat{s}_{eh} = \begin{pmatrix} e^{i\chi_{ehL}} & 0 \\ 0 & e^{i\chi_{ehR}} \end{pmatrix}$$

$$\mathbf{a}_h = \begin{pmatrix} a_{Lh} \\ a_{Rh} \end{pmatrix} = \hat{s}_{he} \begin{pmatrix} b_{Le} \\ b_{Re} \end{pmatrix}$$

$$\begin{pmatrix} \mathbf{a}_e \\ \mathbf{a}_h \end{pmatrix} = \begin{pmatrix} 0 & \hat{s}_{eh} \\ \hat{s}_{he} & 0 \end{pmatrix} \begin{pmatrix} \mathbf{b}_e \\ \mathbf{b}_h \end{pmatrix}$$

Tells how b amplitudes  
are converted into a amplitudes

# Circular relation

$$\begin{pmatrix} \mathbf{b}_e \\ \mathbf{b}_h \end{pmatrix} = \begin{pmatrix} \hat{S}_e & 0 \\ 0 & \hat{S}_h \end{pmatrix} \begin{pmatrix} \mathbf{a}_e \\ \mathbf{a}_h \end{pmatrix}$$

$$\begin{pmatrix} \mathbf{a}_e \\ \mathbf{a}_h \end{pmatrix} = \begin{pmatrix} 0 & \hat{S}_{eh} \\ \hat{S}_{he} & 0 \end{pmatrix} \begin{pmatrix} \mathbf{b}_e \\ \mathbf{b}_h \end{pmatrix}$$

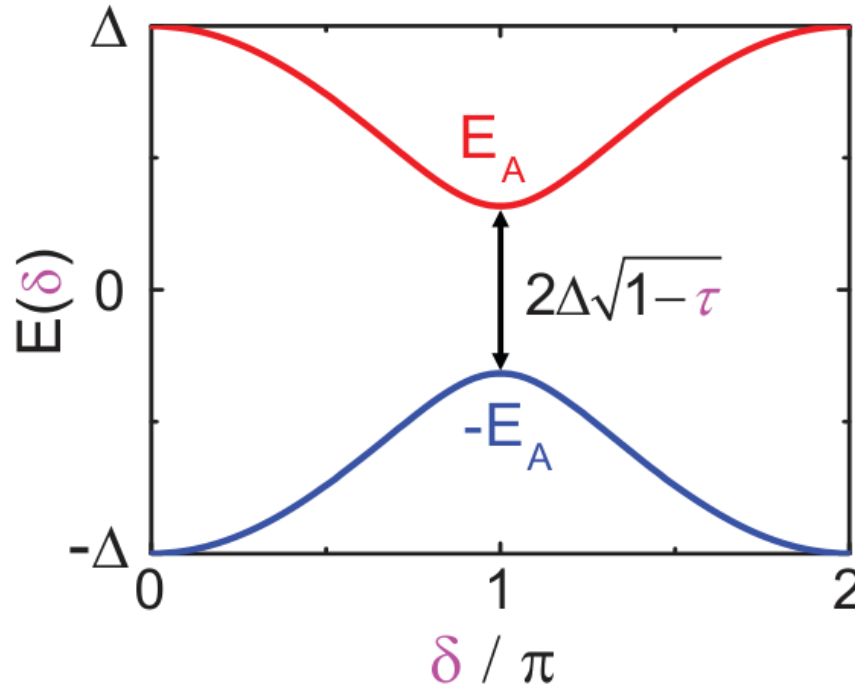
We have to end up in the state where we started

$$\begin{pmatrix} \mathbf{b}_e \\ \mathbf{b}_h \end{pmatrix} = \begin{pmatrix} \hat{S}_e & 0 \\ 0 & \hat{S}_h \end{pmatrix} \begin{pmatrix} 0 & \hat{S}_{eh} \\ \hat{S}_{he} & 0 \end{pmatrix} \begin{pmatrix} \mathbf{b}_e \\ \mathbf{b}_h \end{pmatrix}$$

Solve for Energy...

Do the algebra in the Wolfram Cloud

# Energy of the Andreev Bound State



$$\pm E_A(\delta, \tau) = \pm \Delta \sqrt{1 - \tau \sin^2(\delta/2)}$$

# Current-phase relation for a single channel

$$P = VI = \frac{dE}{dt} = \frac{\partial E}{\partial \gamma} \frac{d\gamma}{dt}$$

$$\frac{d\gamma}{dt} = \frac{1}{\varphi_0} V$$

$$I = \frac{\partial E}{\partial \gamma} \frac{1}{\varphi_0}$$

Exercise: Calculate current across JJ for a single channel of transmission tau

The most general current-phase relation (CPR) for a JJ

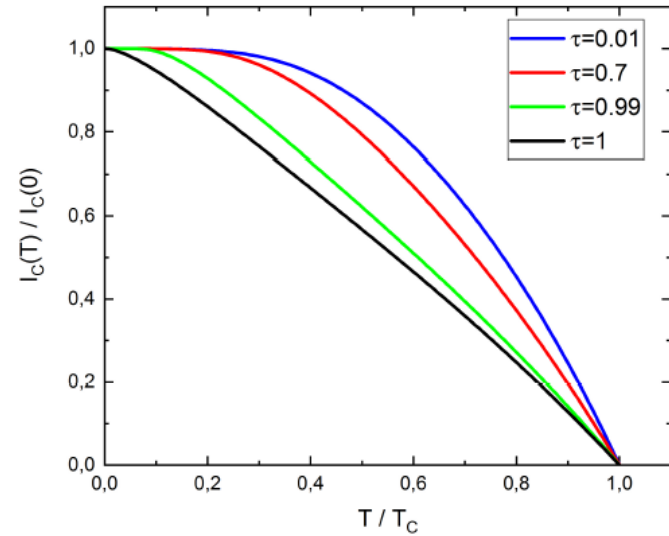
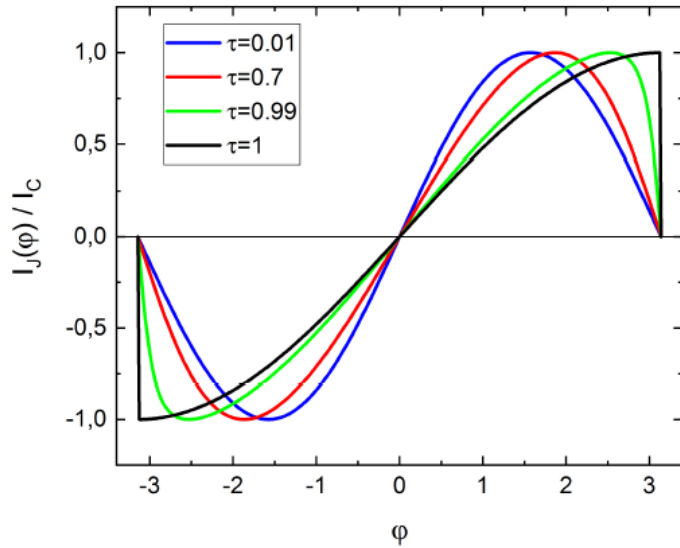
$$I_J(\varphi, T) = \sum_n \frac{e\Delta(T)}{2\hbar} \frac{\tau_n \sin\varphi}{\sqrt{1 - \tau_n \sin^2 \frac{\varphi}{2}}} \tanh \frac{\Delta(T) \sqrt{1 - \tau_n \sin^2 \frac{\varphi}{2}}}{2k_B T}$$

n numbers channels

It reduces to 1st Josephson relation if  $\tau_n \rightarrow 0$  for all channels (tunnel limit):

$$I_J(\varphi) = \frac{\pi\Delta(T)}{2eR_N} \tanh \frac{\Delta(T)}{2k_B T} \sin\varphi = i_c \sin\varphi$$

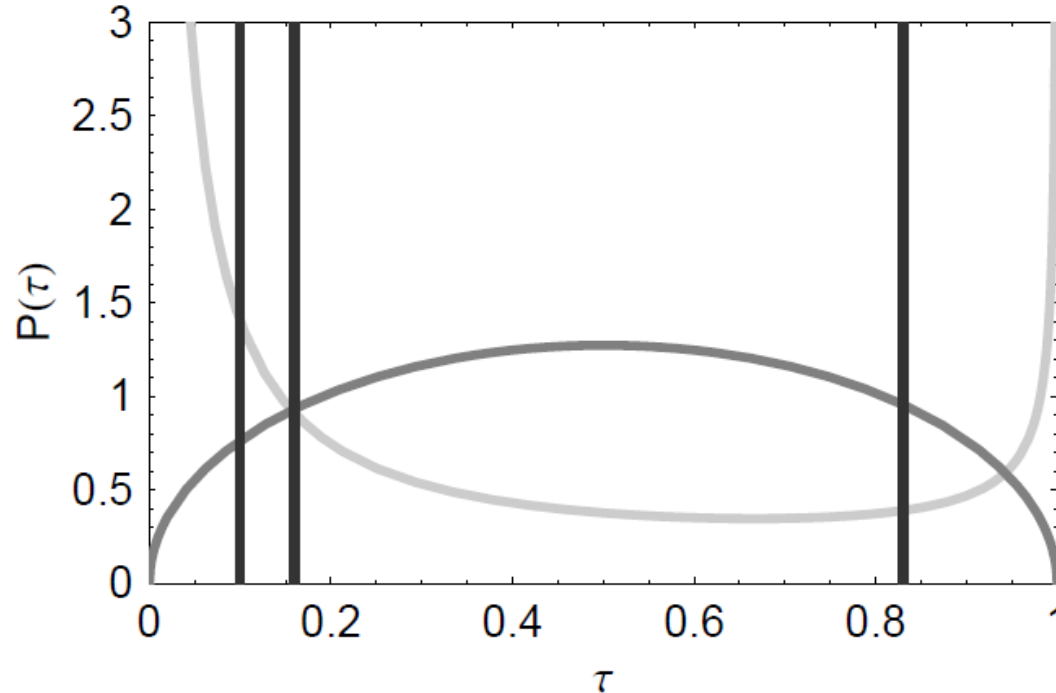
# Single-channel CPRs



$$I_J(\varphi) = N_{\text{ch}} \frac{e\Delta(T)}{2\hbar} \frac{\tau \sin \varphi}{\sqrt{1 - \tau \sin^2 \frac{\varphi}{2}}} \tanh \frac{\Delta(T) \sqrt{1 - \tau \sin^2 \frac{\varphi}{2}}}{2k_B T}$$



# Diffusive weak link: Dorokhov distribution of channel transmissions



$$I(\delta) = M \int_0^1 I_\tau(\delta) P(\tau) d\tau = \frac{2Ml_e}{3L} \int_0^1 \frac{d\tau}{\tau\sqrt{1-\tau}} I_\tau(\delta)$$

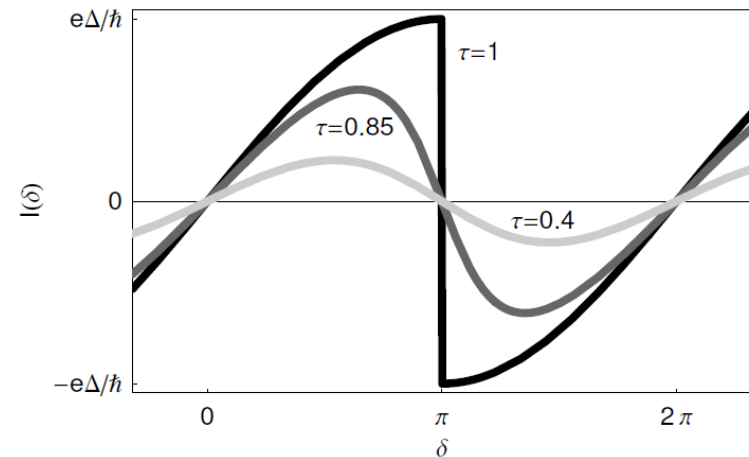
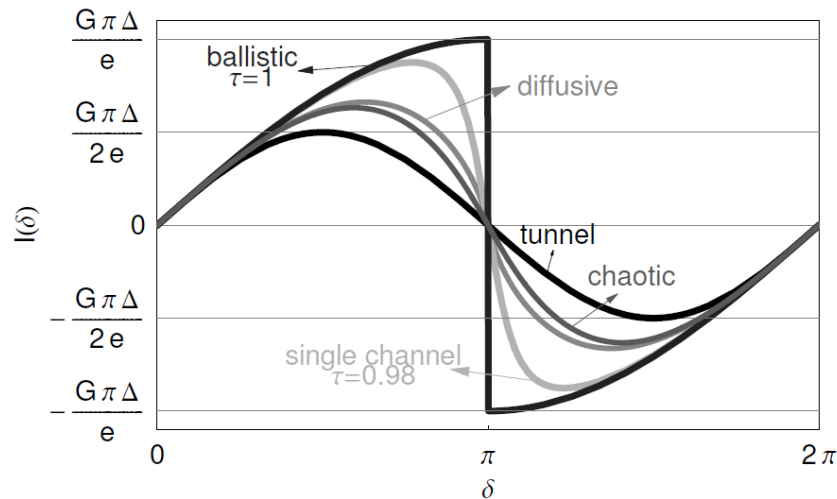
# $I_c R_N$ products

$$I_c(0)R_N = \frac{\pi\Delta}{e}$$

$$I_c(0)R_N = \frac{\pi\Delta}{2e}$$

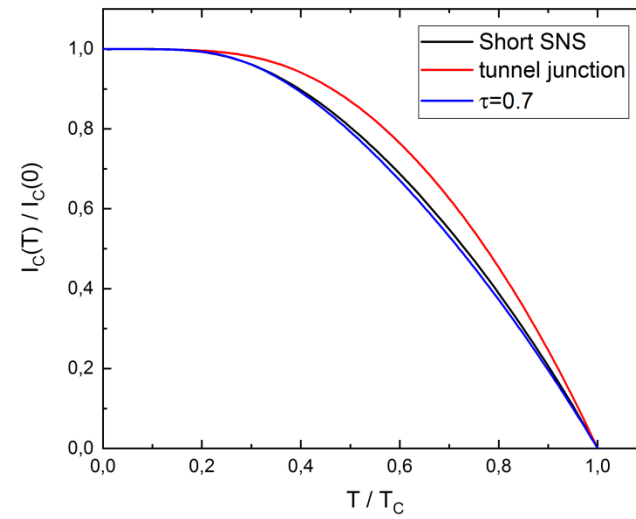
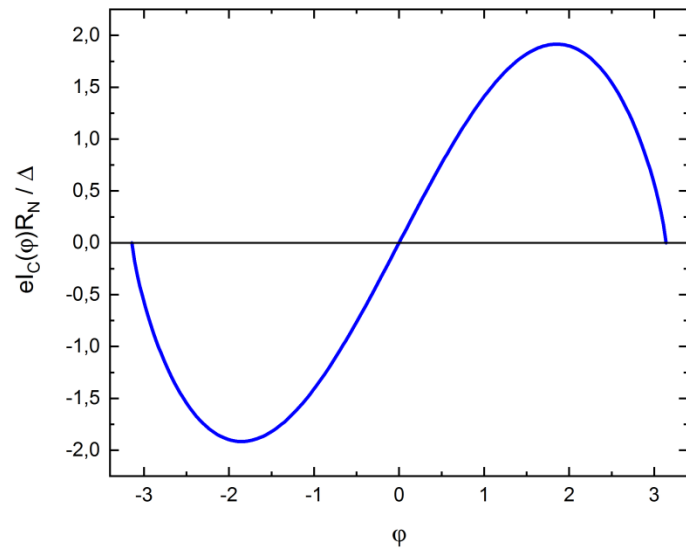
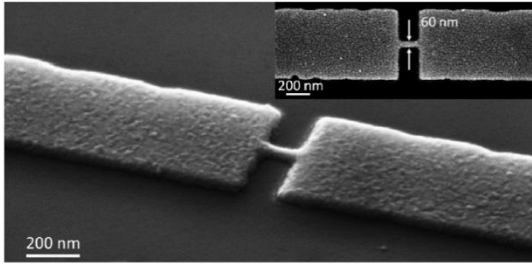
$$I_c(0)R_N = 2.082 \frac{\Delta}{e}$$

$$I_c(0)R_N = \frac{1}{1 + \sqrt{1 - \tau}} \frac{\pi\Delta}{e}$$



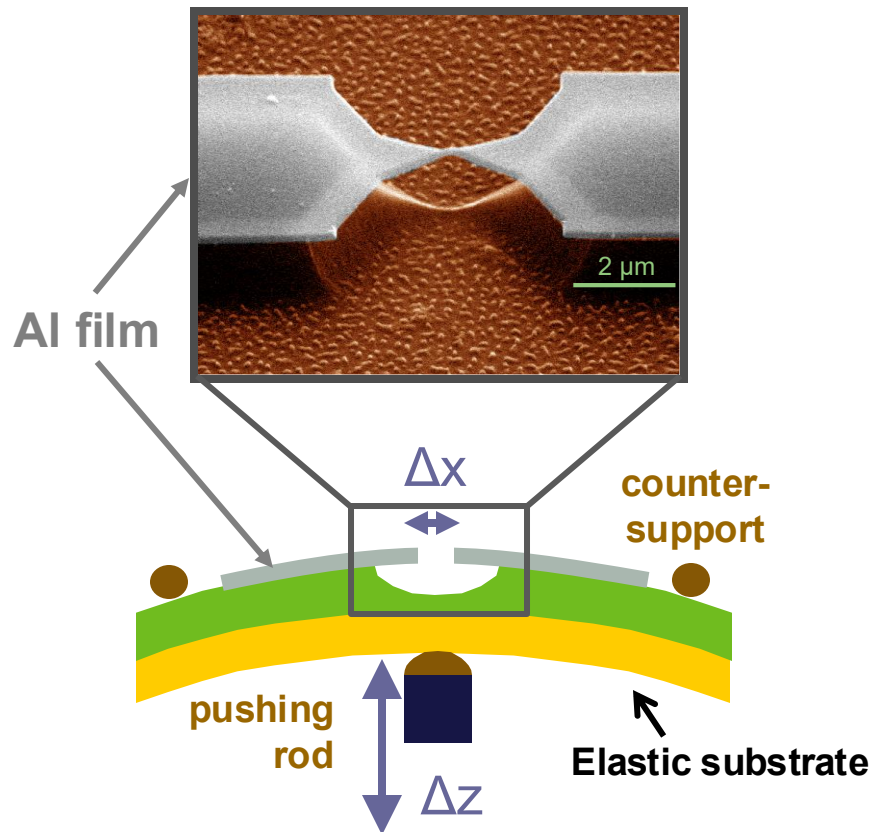
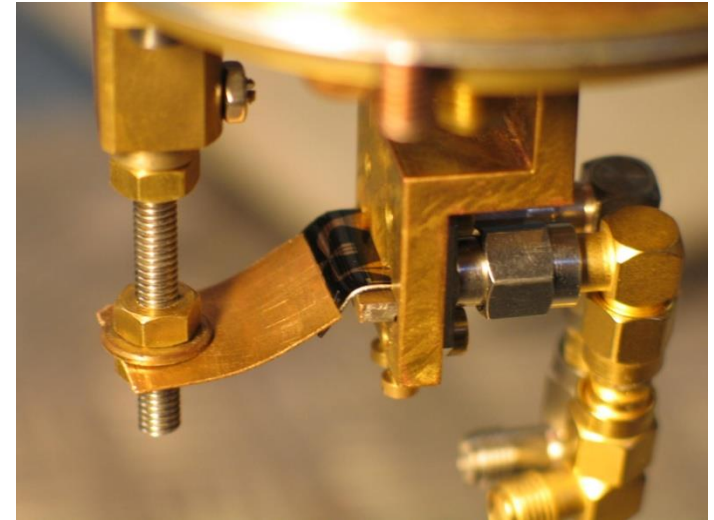
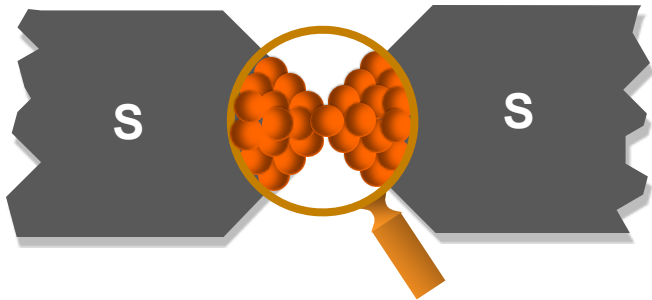
Phase where maximum current is achieved grows with transmission:  
 It is  $\pi/2$  for tunnel junction with  $\tau \rightarrow 0$   
 and  $\pi$  for ballistic channel with  $\tau = 1$ .

# CPR for a diffusive link

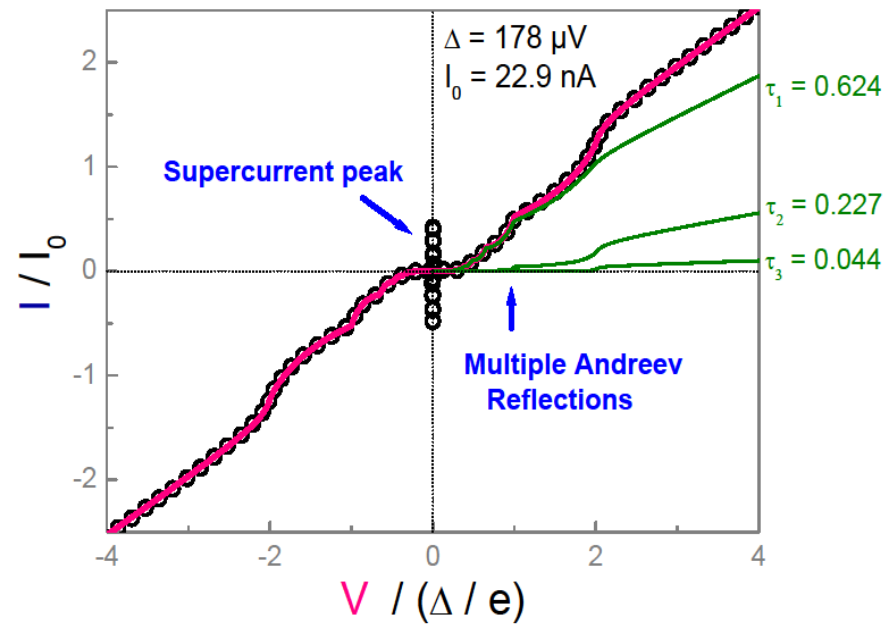


# Atomic contact

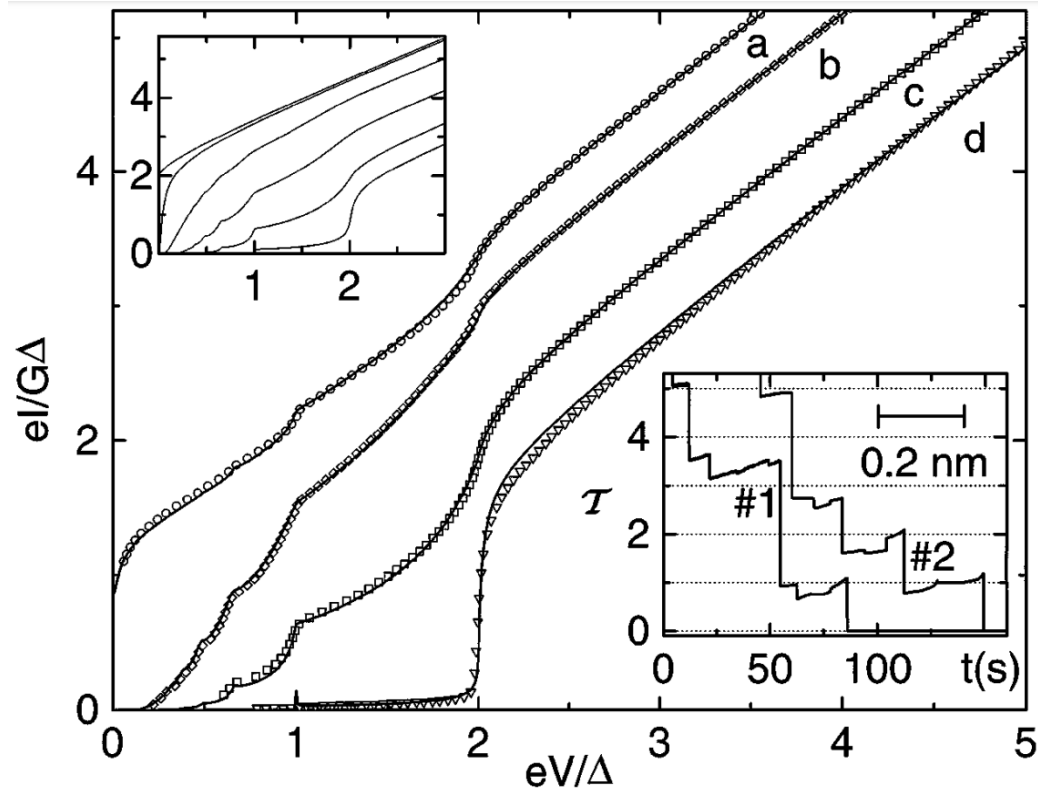
19/19



few channels,  $\{\tau_i\}$  tunable



# Multiple Andreev Reflections (MAR)



The individual channel transmissions and total transmission  $T$  obtained from the fits:

(a)  $\tau_1 = 0.997$ ,  $\tau_2 = 0.46$ ,  $\tau_3 = 0.29$ ,  $T = 1.747$ ;

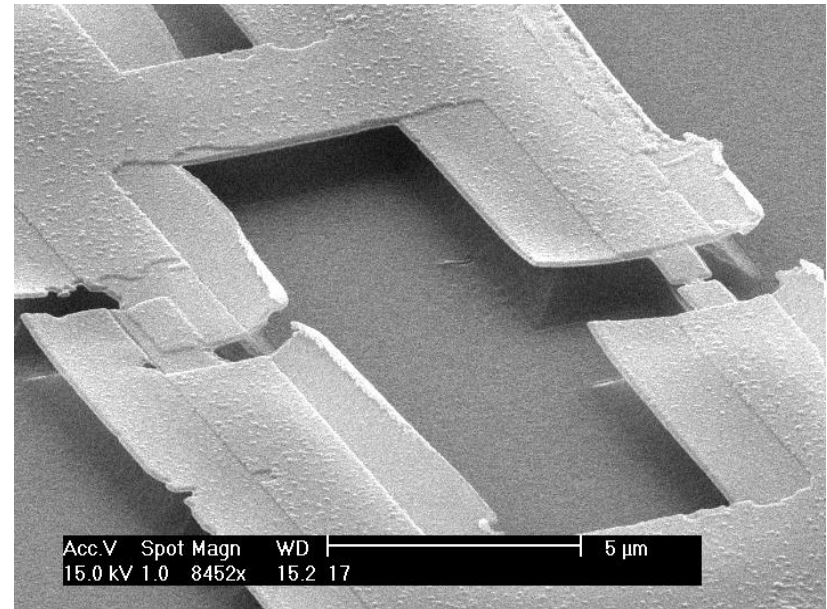
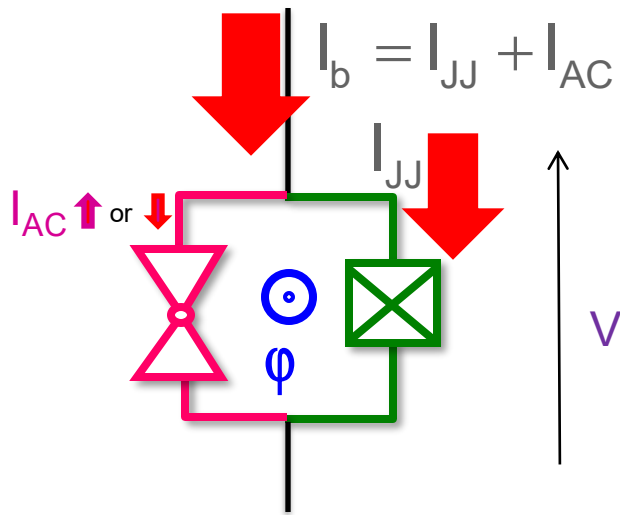
(b)  $\tau_1 = 0.74$ ,  $\tau_2 = 0.11$ ,  $T = 0.85$ ;

(c)  $\tau_1 = 0.46$ ,  $\tau_2 = 0.35$ ,  $\tau_3 = 0.07$ ,  $T = 0.88$ ;

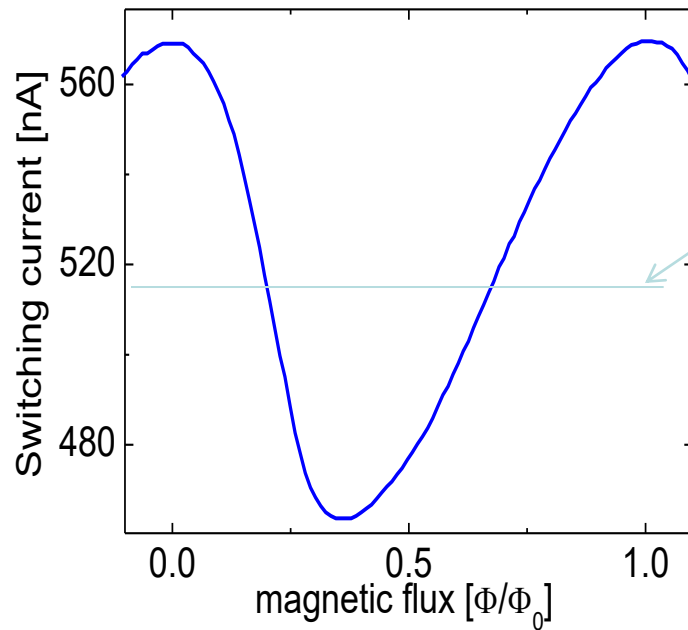
(d)  $T = \tau_1 = 0.025$ .

Phys. Rev. Lett. **78**, 3535 (1997)

# Atomic Squid...- my PostDoc project



# Interference pattern for ATOMIC SQUID



$I_0$ -switching current  
of junction alone

When SQUID switches, phase across  
JJ is the same independently of applied  
magnetic flux  $\Rightarrow$  interference pattern  
is current-phase relation of atomic  
contact



# Coolphon Group:



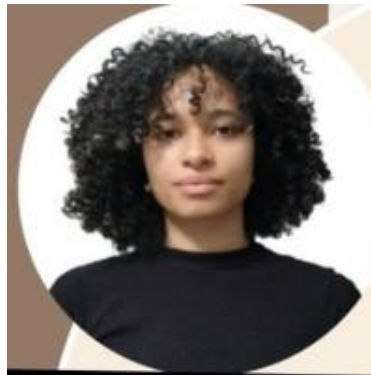
Marek Foltyn, IF PAN



Konrad Norowski, IF PAN



Mujeeb Ahmed, IF PAN



Alissa Aouba, IFPAN/Grenoble

Collaboration:

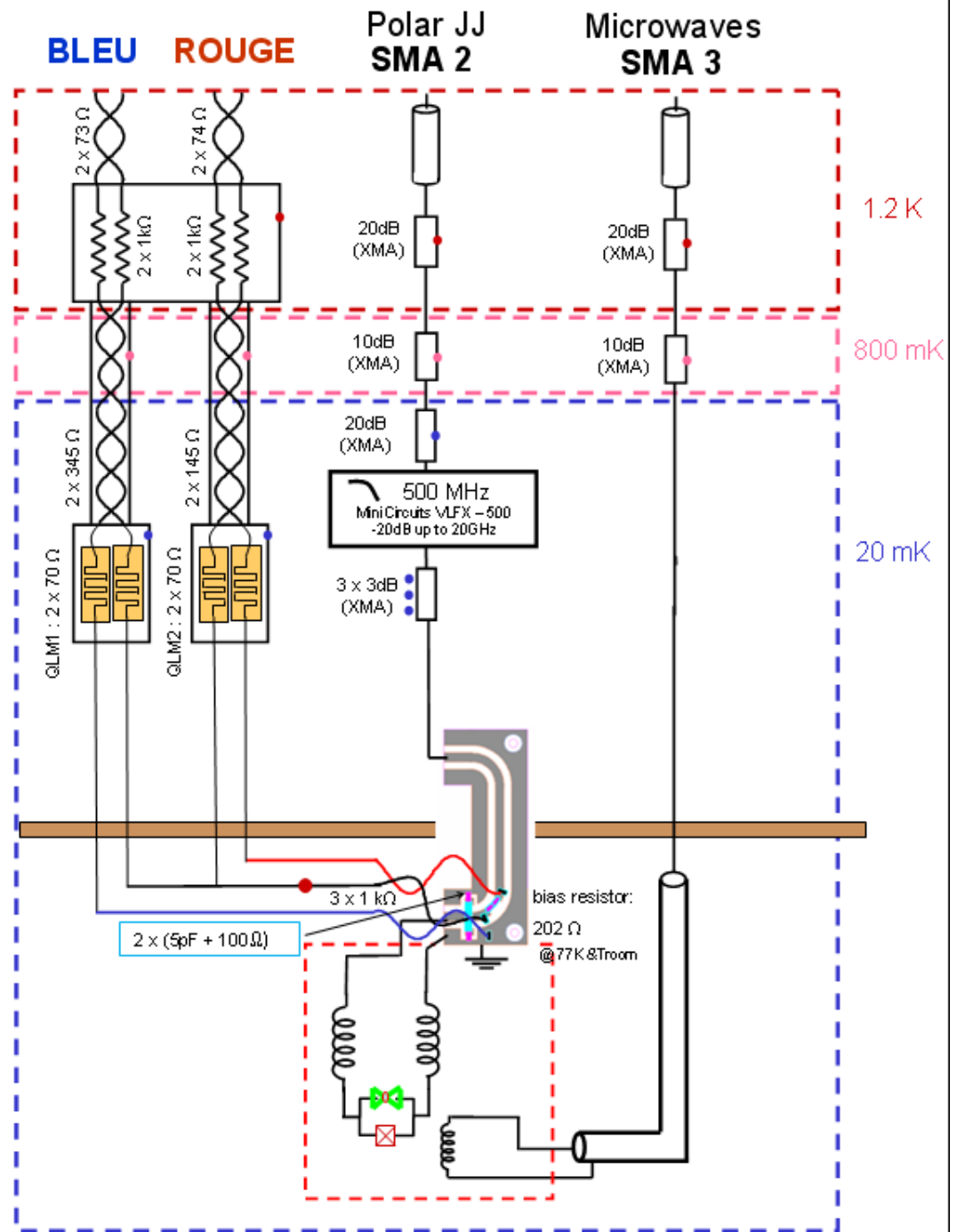


Alexander Savin,  
LTL, Aalto Univ.

Watch us at:

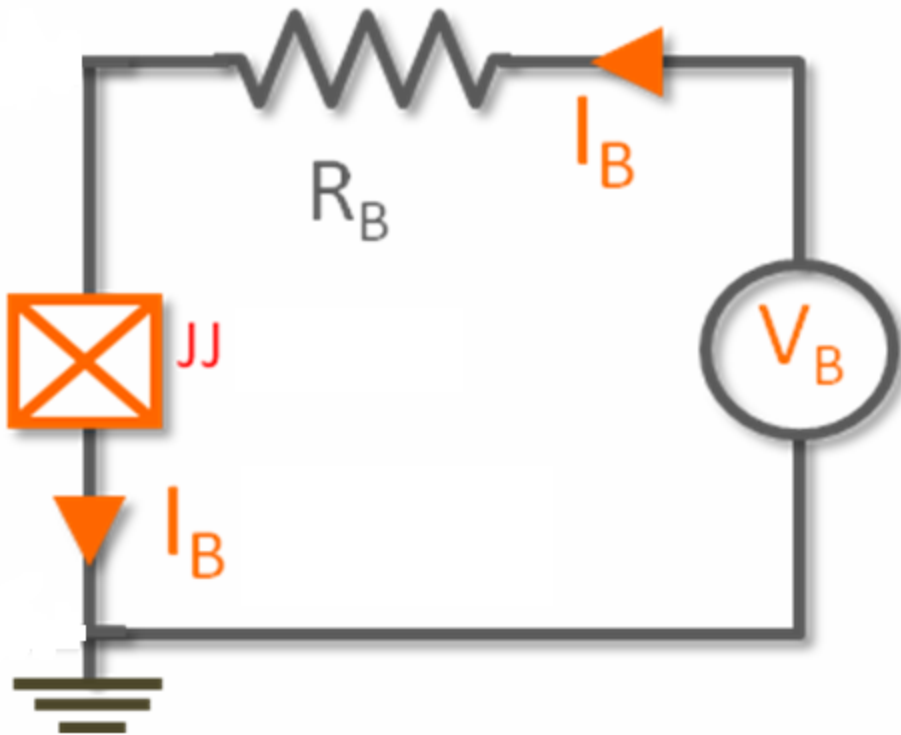
<http://coolphongroup.ifpan.edu.pl>

# Fridge wiring

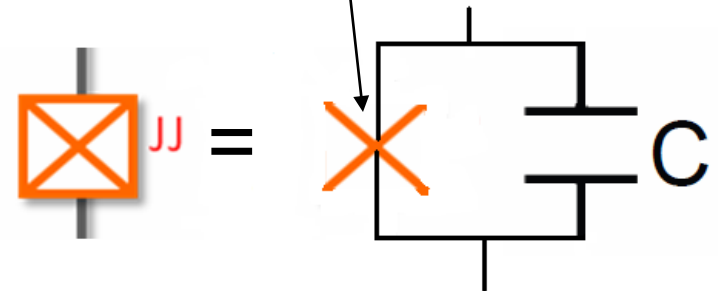


# Electrical circuit

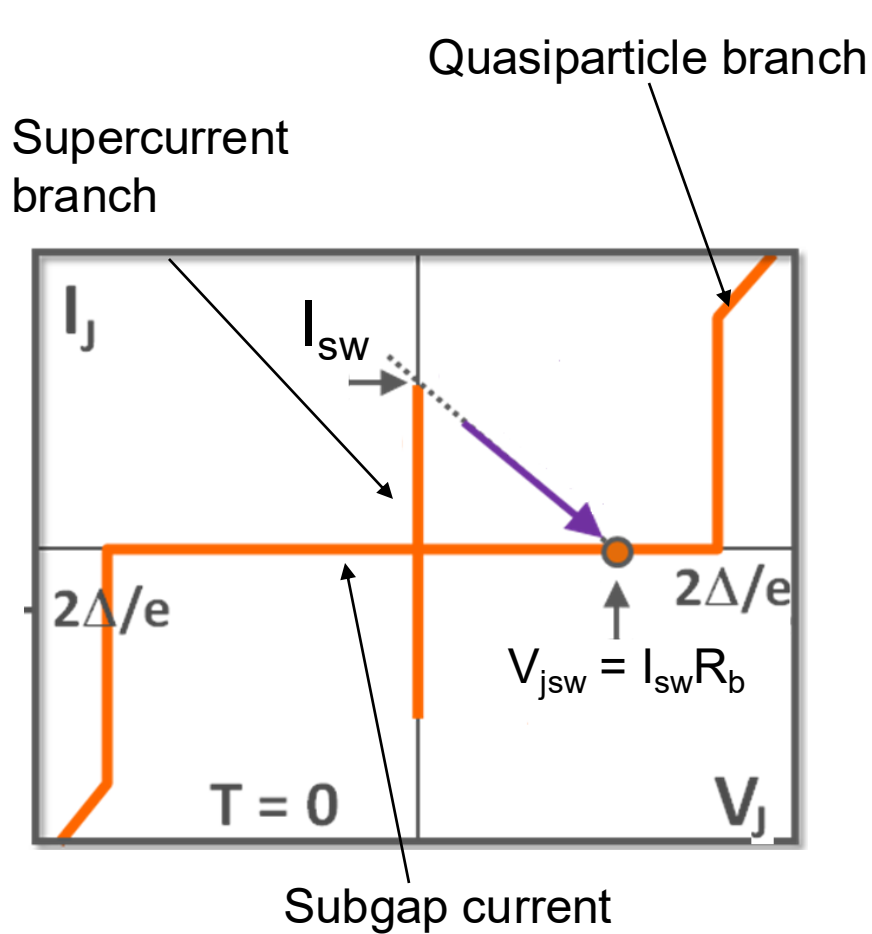
Thevenin equivalent



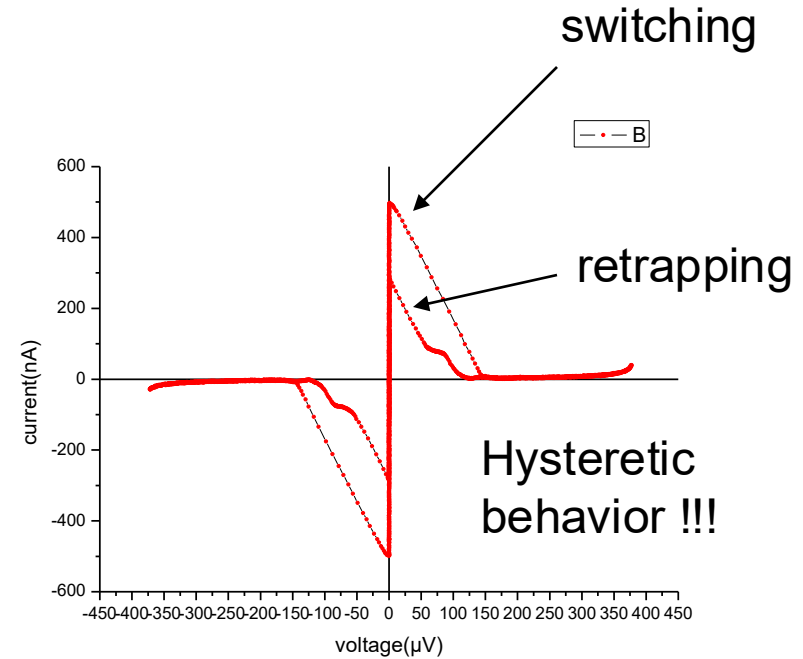
Pure Josephson element  
obeying Josephson relations



# IV curve



*I-V characteristics of JJ biased through  $R_B$  bias resistor. JJ supports supercurrent only to certain level. On crossing the threshold value  $I_0$  finite voltage develops across JJ.*



$$I_j = I_j(V_j)$$

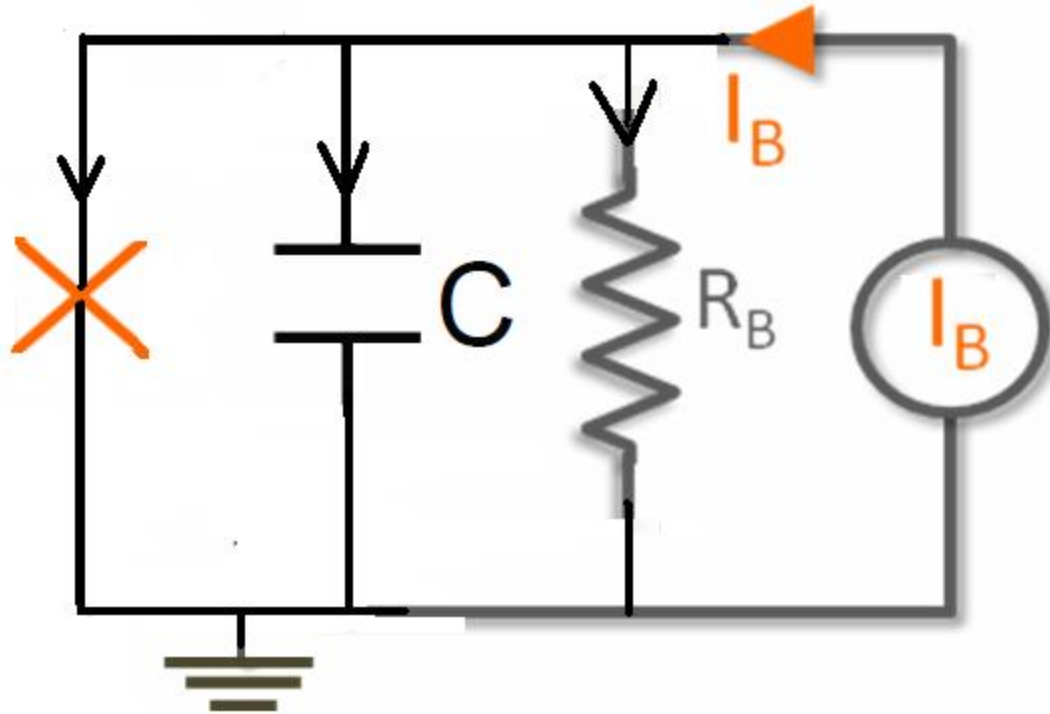
$$V_B = I_j \cdot R_b + V_j \Rightarrow I_j = -\frac{1}{R_b} \cdot V_j + \frac{1}{R_b} \cdot V_b \text{ (load line)}$$

$$\text{At switching } V_j = 0, V_b = V_{bsw} \text{ and } I_j = I_{sw} = \frac{V_{bsw}}{R_b}$$

$$I_j = -\frac{1}{R_b} \cdot V_j + I_{sw} \text{ (switching line)}$$

# RCSJ model

(Resistively and Capacitively Shunted Junction)



$$I_b = I_R + I_C + I_{JJ} = \frac{V}{R} + C \frac{dV}{dt} + I_0 \cdot \sin \gamma$$

# RCSJ model

$$I_b = I_R + I_C + I_{JJ} = \frac{V}{R} + C \frac{dV}{dt} + I_0 \cdot \sin \gamma$$

$$\dot{\gamma} = \frac{1}{\varphi_0} \cdot V$$

$$I_b = \frac{\varphi_0}{R} \dot{\gamma} + C \varphi_0 \ddot{\gamma} + I_0 \sin \gamma$$

First, consider  $\gamma \rightarrow 0$ ,  $I_b = 0$  and map it into harmonic oscillator:

$$C \varphi_0^2 \ddot{\gamma} + \frac{\varphi_0^2}{R} \dot{\gamma} + \varphi_0 I_0 \gamma = 0$$

$$m = C \varphi_0^2, \quad \omega_0 = \left( \frac{I_0}{C \cdot \varphi_0} \right)^{1/2}, \quad b = \frac{\varphi_0^2}{R}, \quad Q_0 = \frac{\omega_0}{b/m} = RC \omega_0, \quad k = \varphi_0 I_0 = E_J$$

Back to full equation:

$$\ddot{\gamma} + \frac{\omega_0}{Q_0} \dot{\gamma} + \omega_0^2 (\sin \gamma - \frac{I_b}{I_0}) = 0$$

Harmonic oscillator:

$$m \ddot{x} + b \dot{x} + kx = 0$$

$$E(t) = E_0 e^{-\gamma t} \text{ (energy of damped harmonic oscillator)}$$

$$\gamma = \frac{b}{m}, \quad Q = \frac{\omega_0}{\gamma}, \quad -kx = -\nabla E_p$$

$$\ddot{x} + \frac{\omega_0}{Q} \dot{x} + \omega_0^2 x = 0$$

**Q - quality factor**, amplitude of harmonic oscillator falls by a factor of e in  $Q/\pi$  cycles of free oscillations

$$\ddot{\gamma} + \frac{\omega_0}{Q_0} \dot{\gamma} + \omega_0^2 \left( \sin \gamma - \frac{I_b}{I_0} \right) = 0$$

Wygląda jak harmonic oscillator, ale teraz restoring force wynosi nie  $k\gamma$  (jak w prawie Hooke'a) tylko:

$$F = -k \left( \sin \gamma - \frac{I_b}{I_0} \right) = -\nabla E_p$$

$$E_p = +k \int \left( \sin \gamma - \frac{I_b}{I_0} \right) d\gamma = -E_J \left( \cos \gamma + \frac{I_b}{I_0} \gamma \right) \quad \textit{tilted washboard potential}$$



# Tilted washboard potential

$$E_p = -E_J \left( \cos \gamma + \frac{I_b}{I_0} \gamma \right)$$

$$\gamma \leftrightarrow x$$

$$V/\phi_0 \text{ (napięcie)} \leftrightarrow v \text{ (prędkość)}$$

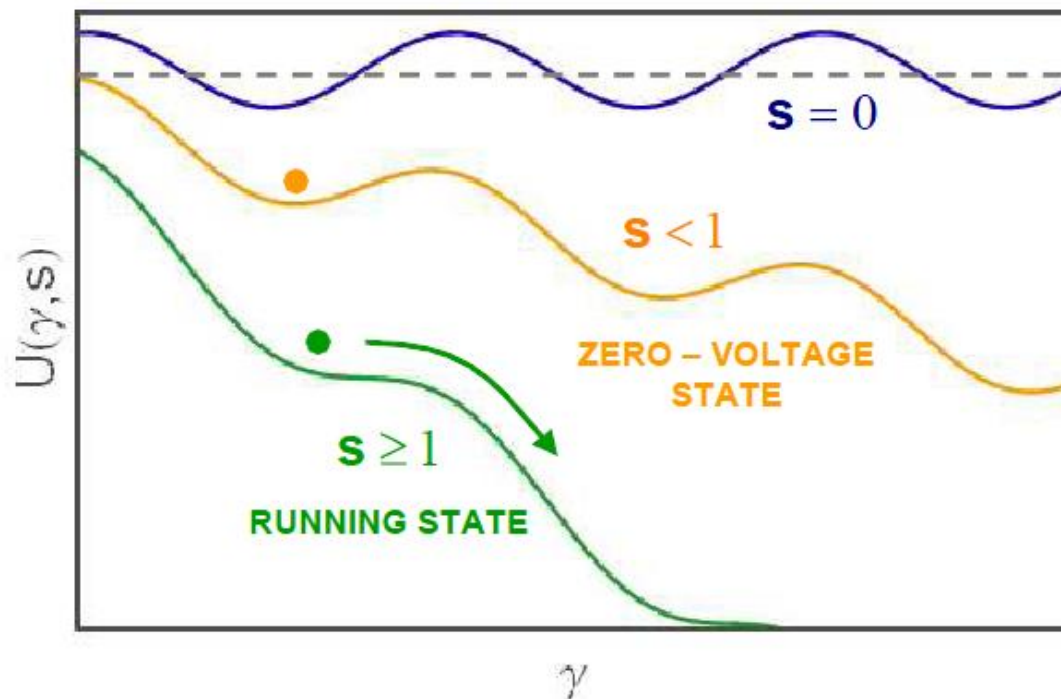


Fig. 2.3. Tilted washboard potential associated to the dynamics of the phase in absence of fluctuations (zero temperature in this classical model). For  $s \leq 1$ , the potential presents wells in which the particle is trapped. For  $s \geq 1$ , the wells disappear and the particle gets into to a running state.

# Q (quality factor) $\leftrightarrow$ hysteresis

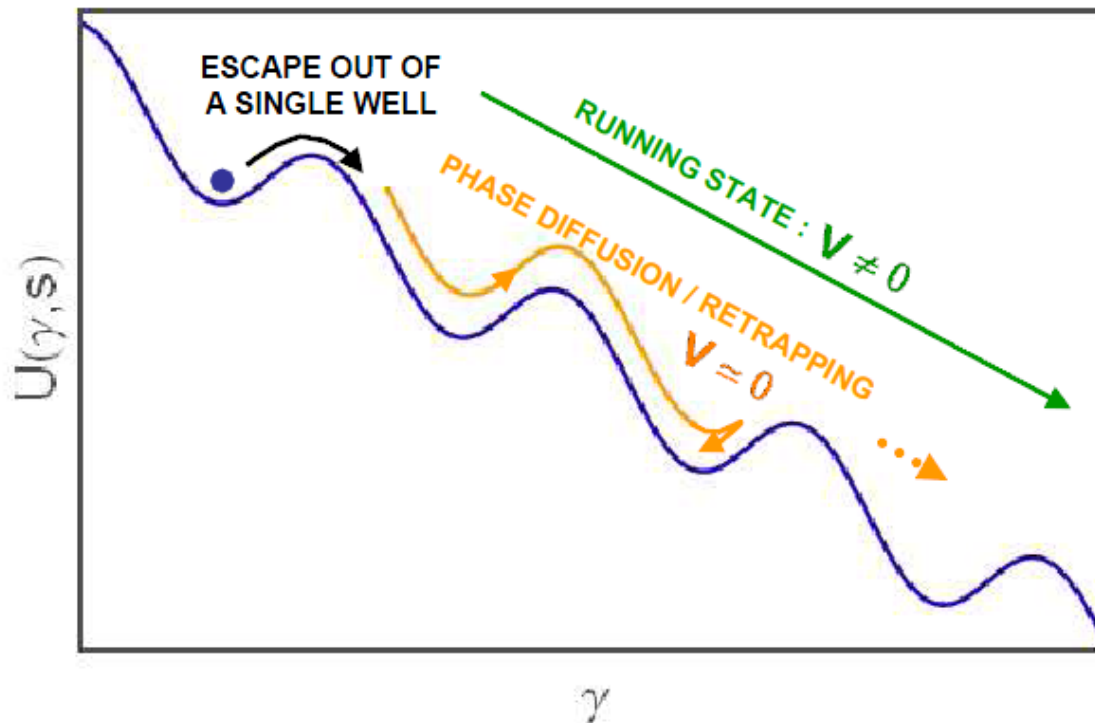


Fig. 2.4. Dynamics of the particle in presence of fluctuations (finite temperature in this classical model). The particle can overcome the barrier and escape out of the single well. The dynamics of the particle depends on the damping. If the damping is small, the particle gains enough energy to reach a running state, leading to a finite voltage. Otherwise, the particle enters a diffusion regime, escaping from one well to be retrapped in a following one, with a very small average velocity.